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MATERIALS ENGINEERING

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Composite
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Micro-CT based permeability calculations with a limited size of the model volume

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FPCM-15
2023

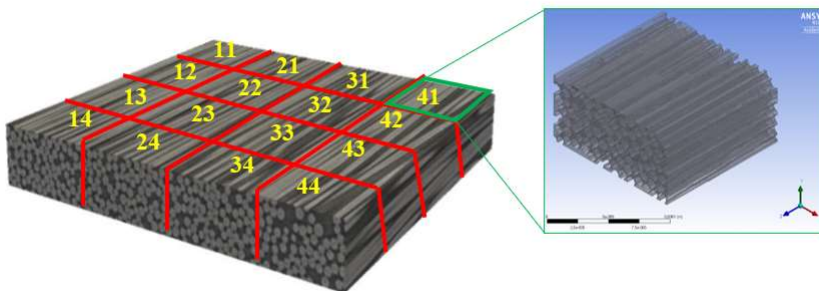
www.composites-kuleuven.be



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Sub-volumes for permeability calculations

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$$K_{i,j,k} = \begin{bmatrix} k_x & 0 & 0 \\ 0 & k_y & 0 \\ 0 & 0 & k_z \end{bmatrix}_{i,j,k}$$

Averaging

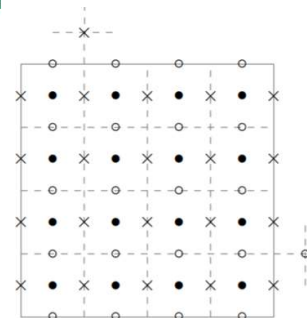
$$K_X = A_{j,k} \left(H_i(k_{X i,j,k}) \right)$$

$$K_Y = A_{i,k} \left(H_j(k_{Y i,j,k}) \right)$$

$$K_Z = A_{i,j} \left(H_k(k_{Z i,j,k}) \right)$$

Darcy solution

$$K_1 = \frac{\langle v_{inlet} \rangle L \mu}{dP}$$



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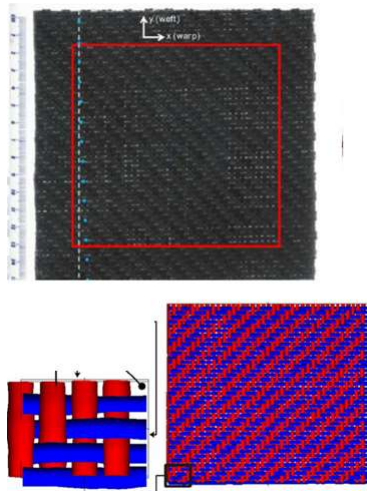
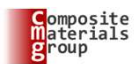
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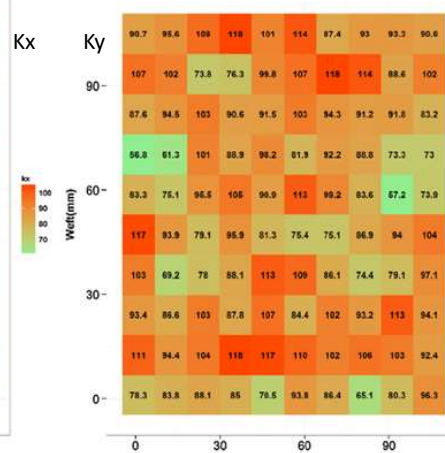
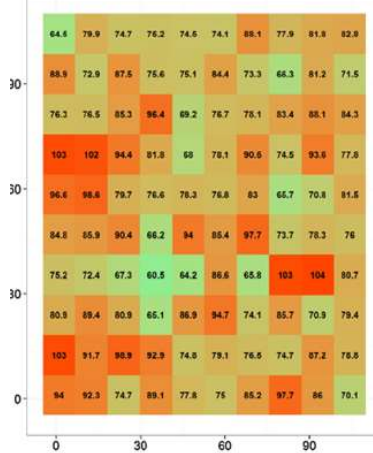
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Example of similar use: variability



Random unit cells comprise a virtual sheet of fabric.



Spatial distribution of permeability of random unit cells. Homogenisation done using A- and H-averaging

FPCM-15 2023 [Bodaghi, M., A. Vanaerschot, S. V. Lomov and N. Correia (2017) Comp A 101: 394-407]



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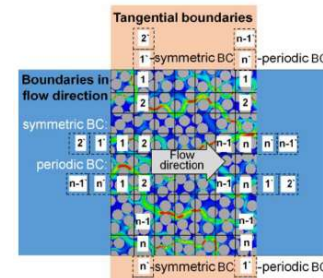
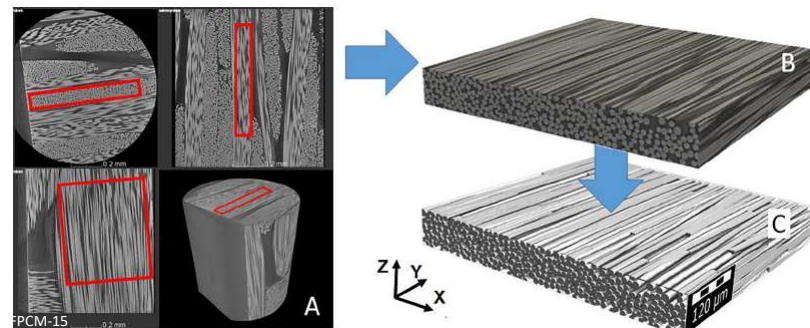
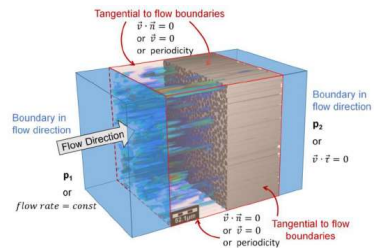
Virtual permeability benchmark



Composites: Part A 167 (2023) 107397

Benchmark exercise on image-based permeability determination of engineering textiles: Microscale predictions

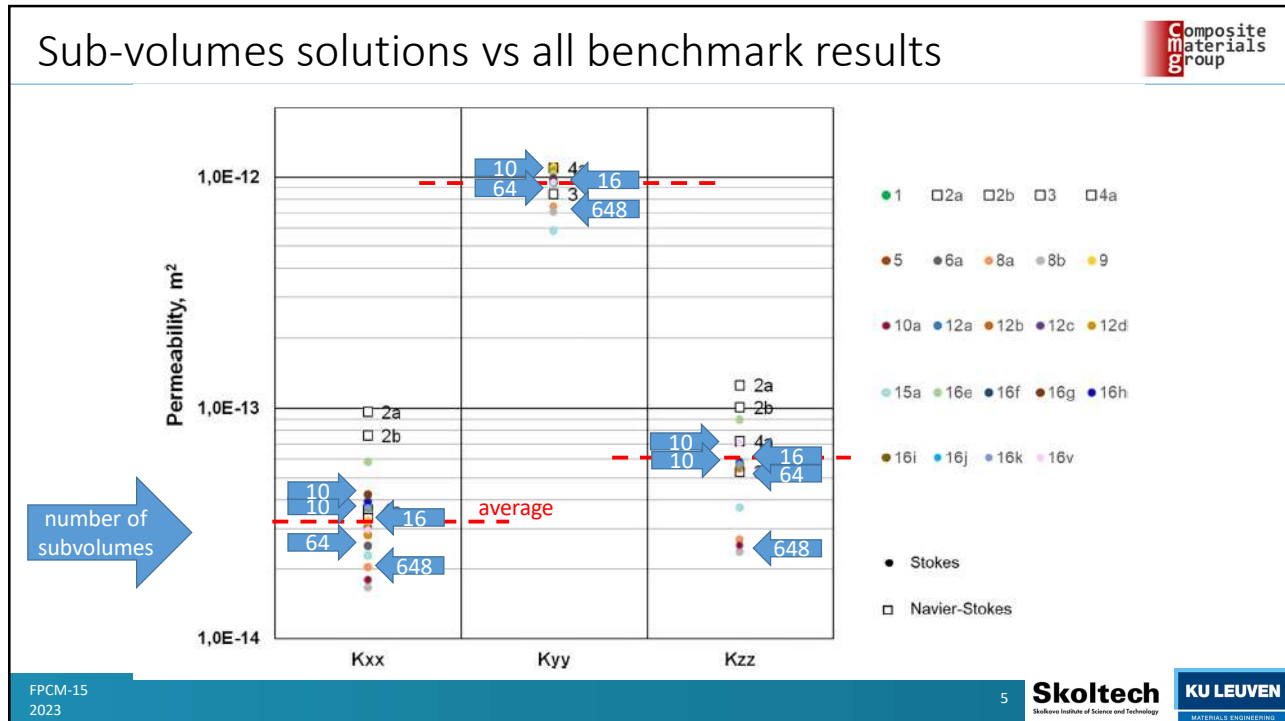
E. Syerko^{a,c}, T. Schmidt^b, D. May^b, C. Binetruy^{a,c}, S.G. Advani^{c,a}, S. Lomov^{d,e}, L. Silva^a, S. Abaimov^e, N. Aissa^a, I. Akhatov^e, M. Ali^f, N. Asiaban^g, G. Broggi^h, J. Bruchonⁱ, B. Caglar^h, H. Digonnet^a, J. Dittmann^j, S. Drapierⁱ, A. Endruweitⁱ, A. Guilloux^m, R. Kandinskii^d, A. Leygue^a, B. Mahato^e, P. Martínez-Leraⁿ, M. Matveev^l, V. Michaud^h, P. Middendorf^j, N. Moulinⁱ, L. Orgéas^k, C.H. Park^o, S. Rief^p, M. Rouhi^{q,t}, I. Sergeichev^e, M. Shakoor^o, O. Shishkinaⁿ, Y. Swolfs^d, M. Tahani^g, R. Umer^f, K. Vancloosterⁿ, R. Vorobyev^e



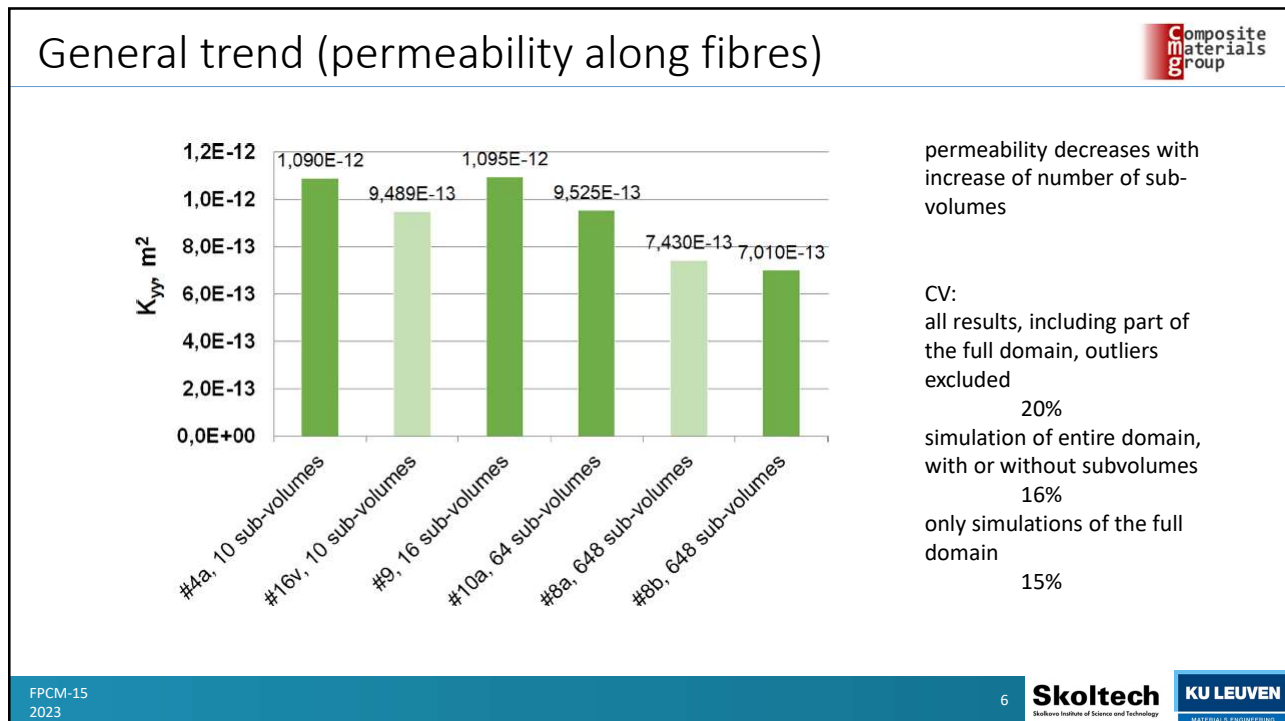
FPCM-15 0.2 mm



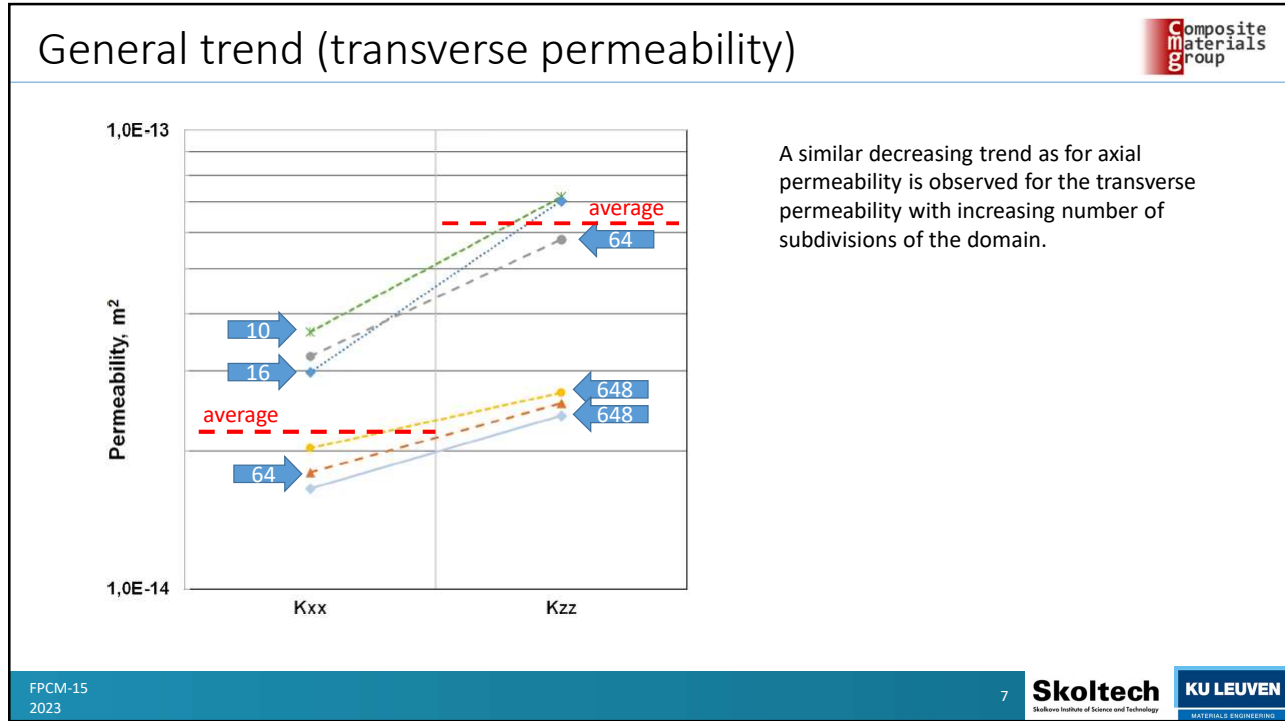
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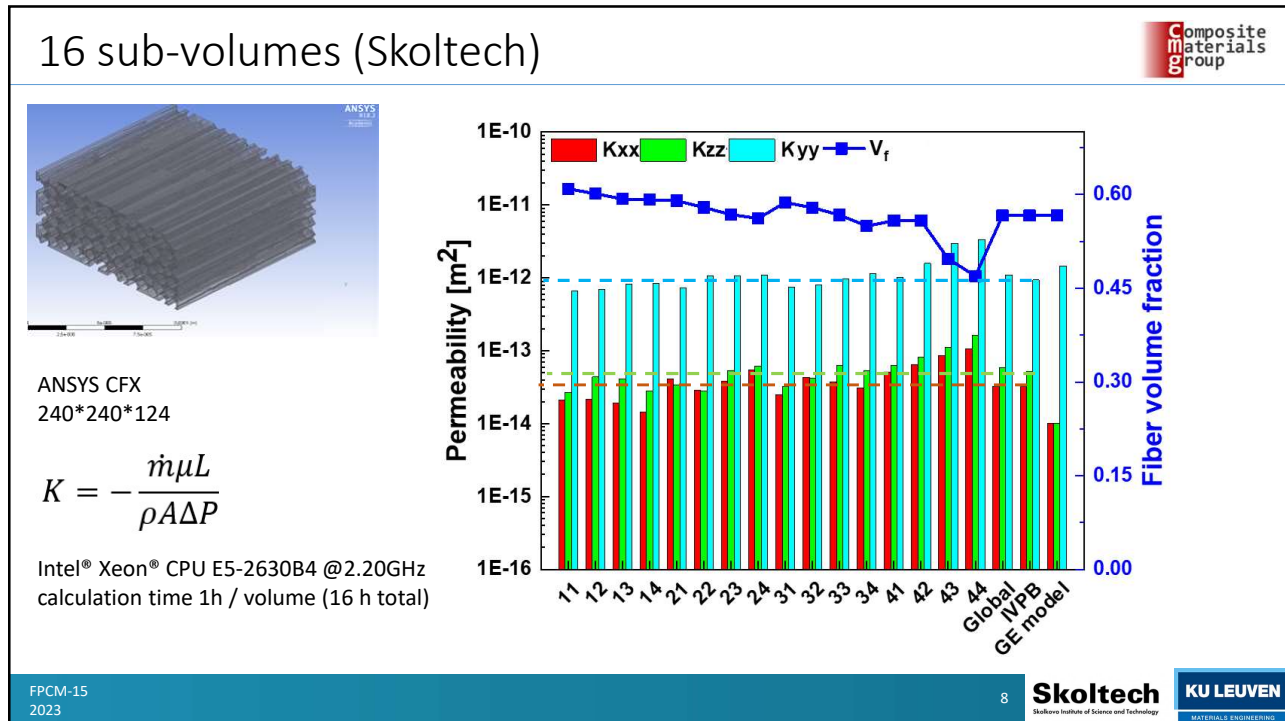
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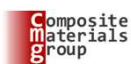


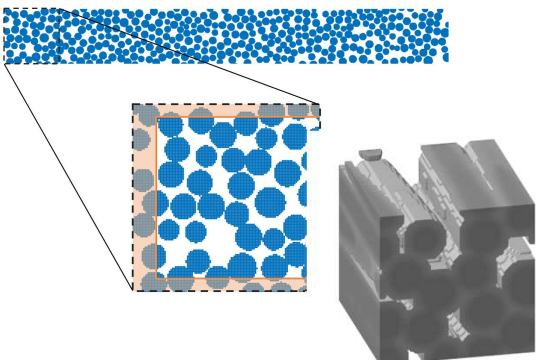
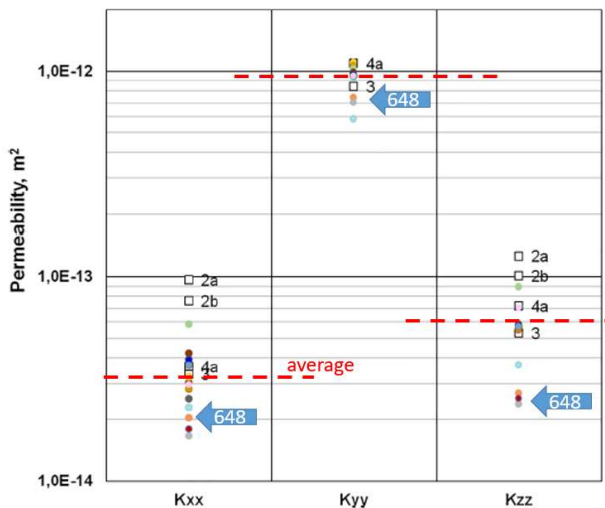
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648 sub-volumes (KU Leuven)





FlowTex (KU Leuven): finite difference Stokes solver
 strong model size limitation (~ 800,000 voxels)
 54*54*54 voxels
 18*18*2 = 648 sub-volumes

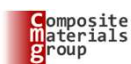
Intel® Core™ i5-8350U CPU @ 1.70GHz
 time for a sub-volume ~ 30 s, total per volume 5.5 h.

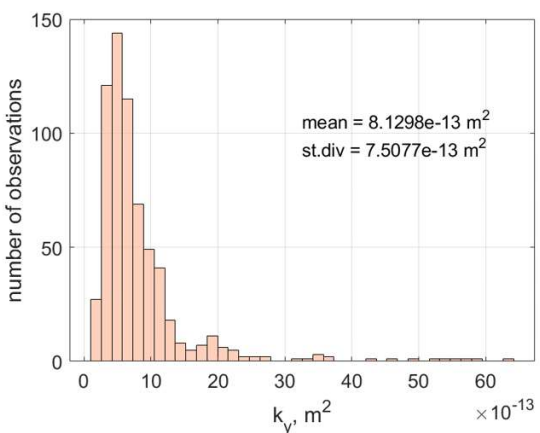
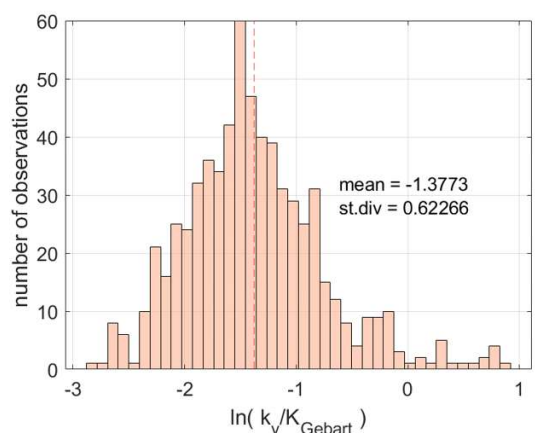
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Distribution of sub-volume permeability (along fibres)



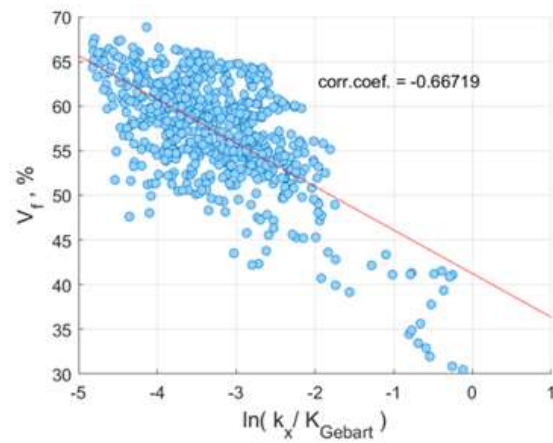
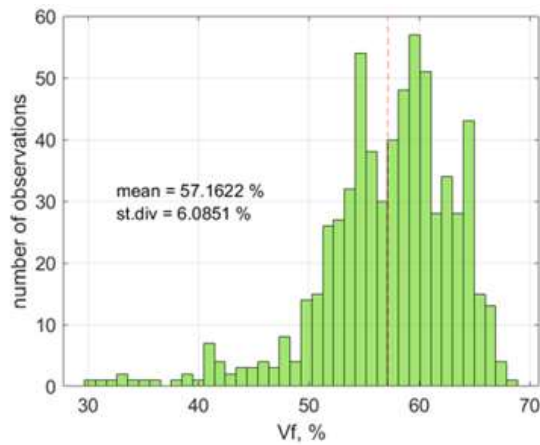



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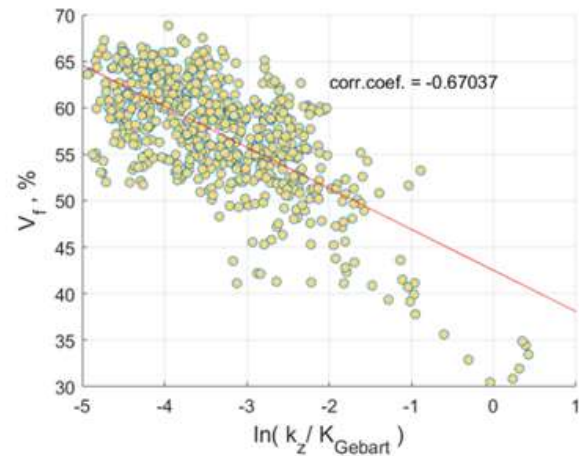
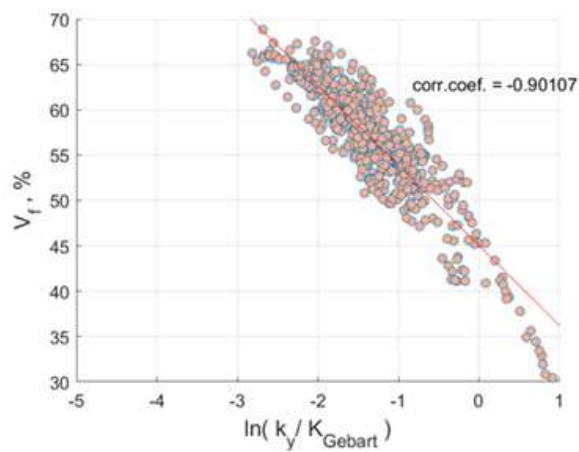
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Correlation with fibre volume fraction – 1



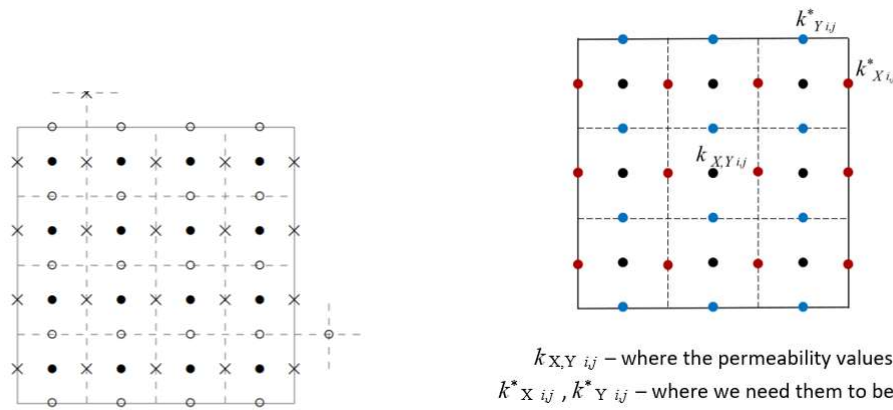
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Correlation with fibre volume fraction – 2



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Darcy averaging – 1

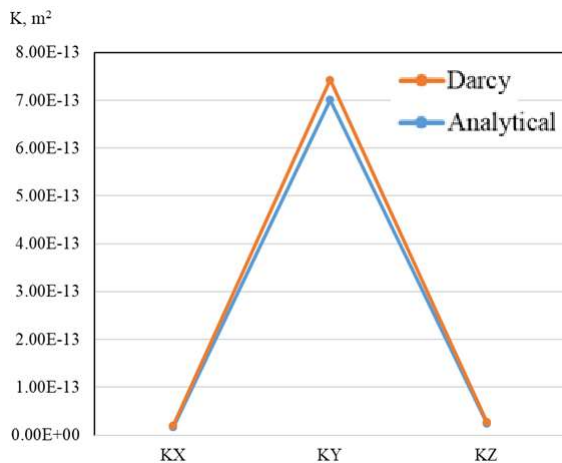


Staggered grid location of unknowns for the MAC scheme. The discrete pressure p is defined at cell centers (\bullet). The discrete velocity u and v are defined at vertical edges centers (\times) and horizontal edges centers (\circ), respectively.

[Wang, Chen *J Sci Comp* 2013]

interpolation to get k 's in the staggered nodes

Darcy averaging – 2



	Analytical	Darcy	average benchmark
KX	1.7×10^{-14}	2.0×10^{-14}	3.2×10^{-14}
KY	7.0×10^{-13}	7.4×10^{-13}	9.4×10^{-13}
KZ	2.4×10^{-14}	2.7×10^{-14}	5.2×10^{-14}

	Analytical	Darcy	average benchmark
KY/KX	42	36	29
KY/KZ	29	28	18

Conclusions



BENCHMARK PAPER

- **The higher the number of cropped sub-volumes**, i.e. the higher the number of artificial boundaries introduced into the domain, **the lower the predicted permeability is**.
- Calculating the permeability of the entire sample by **this renormalization approach can be a good solution if the number of sub-volumes is not too high** and in cases where the computational resources are limited in terms of memory or time.
- The minimal number of sub-volumes (10) used in the benchmark study resulted in **only 15% deviation** from the cluster average value.

DARCY HOMOGENISATION

- Darcy homogenisation of subdomains is **very close** to the analytical “arithmetic – harmonic mean”
- Analytical averaging cannot represent the skew terms of **K** tensor; **Darcy can**.

Acknowledgements



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